# Kinematics $C^{\circ}$ Dynamics of Linkages Lecture 13: 3 Positions Analytical Synthesis 

## 3-Pasition Mation Generation with Fixed Pivots

Design a four bar linkage that will mave a line on its coupler link such that a point $P$ on that line will be first at $\mathrm{PI}, \mathrm{P} 2$ and later P3 and will Also rotate the line through an angle $\alpha_{2}$ and then $\alpha_{3}$ assuming fixed pivats $\bar{D}_{2}$ and $\mathrm{C}_{4}$


## |st Dyade: WZ

## Define the following variables:

$w=$ length link2
$\boldsymbol{\theta}=$ initial angle of link2
$\boldsymbol{\beta}_{2}=$ |st change in angle of link2
$\boldsymbol{\beta}_{3}=$ 2nd $^{\text {nd }}$ change in angle of link2
$\boldsymbol{z}=$ distance from $\boldsymbol{A}$ and $\boldsymbol{P}$
$\Phi=$ initial angle of link $z$
$\boldsymbol{\alpha}_{2}={ }^{\text {st }}$ change in angle of link $\boldsymbol{z}$
$\boldsymbol{\alpha}_{3}=2^{\text {nd }}$ change in angle of link $\boldsymbol{z}$
$\boldsymbol{p}_{21}=$ distance from point $\boldsymbol{P}_{\boldsymbol{f}}$ to $\boldsymbol{P}_{2}$
$\boldsymbol{\rho}_{31}=$ distance from point $\boldsymbol{P}_{\boldsymbol{f}}$ to $\boldsymbol{P}_{3}$
$\boldsymbol{R}_{f}=$ position vector $\mathrm{D}_{2} \mathrm{P}_{1}$
$\boldsymbol{R}_{2}=$ position vector $\mathrm{D}_{2} \mathrm{P}_{2}$
$R_{3}=$ position vector $\mathrm{D}_{2} \mathrm{P}_{3}$
$\xi_{1}=$ orientation angle of $\boldsymbol{R}_{\text {l }}$
$\xi_{2}=$ orientation angle of $R_{2}$
$\xi_{3}=$ orientation angle of $R_{3}$
$R_{1}=$ magnitude of $\boldsymbol{R}_{\boldsymbol{t}}$
$R_{2}=$ magnitude of $\boldsymbol{R}_{\boldsymbol{z}}$
$R_{3}=$ magnitude of $\boldsymbol{R}_{3}$
$\boldsymbol{\delta}_{2}=$ arientation angle of line from $\boldsymbol{P}_{\boldsymbol{f}}$ to $\boldsymbol{P}_{2}$
$\delta_{3}=$ orientation angle of line from $\boldsymbol{P}_{\text {to }} \boldsymbol{P}_{3}$

## |st Dyade: WZ - Solution

Write the Vectar loup of each precision position

$$
\begin{aligned}
& W_{1}+Z_{1}=R_{1} \\
& W_{2}+Z_{2}=R_{2} \\
& W_{3}+Z_{3}=R_{3}
\end{aligned}
$$

## Substitute

$$
\begin{aligned}
& W_{1}=w e^{j \theta}, W_{2}=w e^{j\left(\theta+\beta_{2}\right)}=W_{1} e^{j \beta_{2}} \\
& Z_{1}=z e^{j \phi}, Z_{2}=z e^{j\left(\phi+\alpha_{2}\right)}=Z_{1} e^{j \alpha_{2}}
\end{aligned}
$$



## |st Dyade: WZ - Solution

Resultant system of equations
$W_{1}+Z_{1} \quad=R_{1}$
$W_{1} e^{j \beta_{2}}+Z_{1} e^{j \alpha_{2}}=R_{2}$
$W_{1} e^{j \beta_{3}}+Z_{1} e^{j \alpha_{3}}=R_{3}$
Solution: determinant of the below matrix is zero
$\left[\begin{array}{ccc}1 & 1 & R_{1} \\ e^{j \beta_{2}} & e^{j \alpha_{2}} & R_{2} \\ e^{j \beta_{3}} & e^{j \alpha_{3}} & R_{3}\end{array}\right]$


## |st Dyade: WZ - Solution

The determinant can be simplified to $A+B e^{j \beta_{2}}+C e^{j \beta_{3}}=0$

Where

$$
\begin{aligned}
& A=R_{3} e^{j \alpha_{2}}-R_{2} e^{j \alpha_{3}} \\
& B=R_{1} e^{j \alpha_{3}}-R_{3} \\
& C=R_{2} \quad-R_{1} e^{j \alpha_{2}}
\end{aligned}
$$



## |st Dyade: WZ - Solution

Solving the real and imaginary part of the equation we get
$\beta_{3}=2 \arctan \left(\frac{K_{2} \pm \sqrt{K_{1}^{2}+K_{2}^{2}-K_{3}^{2}}}{K_{1}+K_{3}}\right)$
$\beta_{2}=\arctan \left[\frac{-\left(A_{3} \sin \beta_{3}+A_{2} \cos \beta_{3}+A_{4}\right)}{-\left(A_{5} \sin \beta_{3}+A_{3} \cos \beta_{3}+A_{6}\right)}\right]$

Ignore the solution where $\beta_{2}=\alpha_{2}$ and $\beta_{3}=\alpha_{3}$


## |st Dyade: WZ - Solution Constants

$K_{1}=A_{2} A_{4}+A_{3} A_{6}$
$K_{2}=A_{3} A_{4}+A_{5} A_{6}$
$K_{3}=\frac{\left(A_{1}^{2}-A_{2}^{2}-A_{3}^{2}-A_{4}^{2}-A_{6}^{2}\right)}{2}$
$A_{1}=-C_{3}^{2}-C_{4}^{2}$
$A_{2}=C_{3} C_{6}-C_{4} C_{5}$
$A_{3}=-C_{4} C_{6}-C_{3} C_{5} \quad A_{4}=C_{2} C_{3}+C_{1} C_{4}$
$A_{5}=C_{4} C_{5}-C_{3} C_{6}$
$A_{6}=C_{1} C_{3}-C_{2} C_{4}$
$C_{1}=R_{3} \cos \left(\alpha_{2}+\zeta_{3}\right)-R_{2} \cos \left(\alpha_{3}+\zeta_{2}\right)$
$C_{2}=R_{3} \sin \left(\alpha_{2}+\zeta_{3}\right)-R_{2} \sin \left(\alpha_{3}+\zeta_{2}\right)$
$C_{3}=R_{1} \cos \left(\alpha_{3}+\zeta_{1}\right)-R_{3} \cos \zeta_{3}$
$C_{4}=-R_{1} \sin \left(\alpha_{3}+\zeta_{1}\right)+R_{3} \sin \zeta_{3}$
$C_{5}=R_{1} \cos \left(\alpha_{2}+\zeta_{1}\right)-R_{2} \cos \zeta_{2}$
$C_{6}=-R_{1} \sin \left(\alpha_{2}+\zeta_{1}\right)+R_{2} \sin \zeta_{2}$

## |st Dyade: WZ

Use the following vector loap equation to solve for $W$ and $Z$

$$
\begin{aligned}
& W_{2}+Z_{2}-P_{21}-Z_{1}-W_{1}=0 \\
& W_{3}+Z_{3}-P_{31}-Z_{1}-W_{1}=0
\end{aligned}
$$

Unknowns

$$
\begin{array}{ll}
W_{1_{x}}=w \cos \theta & Z_{1_{x}}=z \cos \phi \\
W_{1_{y}}=w \sin \theta & Z_{1_{y}}=z \sin \phi
\end{array}
$$

## |st Dyade: WZ

Take the real and imaginary components of bath equations
$A W_{1_{x}}-B W_{1_{y}}+C Z_{1_{x}}-D Z_{1_{y}}=E$
$F W_{1_{x}}-G W_{1_{y}}+H Z_{1_{x}}-K Z_{1_{y}}=L$
$B W_{1_{x}}+A W_{1_{y}}+D Z_{1_{x}}+C Z_{1_{y}}=M$
$G W_{1_{x}}+F W_{1_{y}}+K Z_{1_{x}}+H Z_{1_{y}}=N$

## Where

$A=\cos \beta_{2}-1 \quad B=\sin \beta_{2} \quad C=\cos \alpha_{2}-1$
$D=\sin \alpha_{2} \quad E=p_{21} \cos \delta_{2} \quad F=\cos \beta_{3}-1$
$G=\sin \beta_{3} \quad H=\cos \alpha_{3}-1 \quad K=\sin \alpha_{3}$
$L=p_{31} \cos \delta_{3} \quad M=p_{21} \sin \delta_{2} \quad N=p_{31} \sin \delta_{3}$


## pst Dyade: WZ

Solve the system of equations using matrices
$\left[\begin{array}{cccc}A & -B & C & -D \\ F & -G & H & -K \\ B & A & D & C \\ G & F & K & H\end{array}\right] \times\left[\begin{array}{c}W_{1_{x}} \\ W_{1_{y}} \\ Z_{1_{x}} \\ Z_{1_{y}}\end{array}\right]=\left[\begin{array}{c}E \\ L \\ M \\ N\end{array}\right]$

The matrix solution will give the solution to vectors $W$ and $Z$.
Reda the same procedure far vector $ل$ and $S$

## Solution Summary

$\beta_{3}=2 \arctan \left(\frac{K_{2} \pm \sqrt{K_{1}^{2}+K_{2}^{2}-K_{3}^{2}}}{K_{1}+K_{3}}\right)$
$\beta_{2}=\arctan \left[\frac{-\left(A_{3} \sin \beta_{3}+A_{2} \cos \beta_{3}+A_{4}\right)}{-\left(A_{5} \sin \beta_{3}+A_{3} \cos \beta_{3}+A_{6}\right)}\right]$

$$
\left[\begin{array}{cccc}
A & -B & C & -D \\
F & -G & H & -K \\
B & A & D & C \\
G & F & K & H
\end{array}\right] \times\left[\begin{array}{c}
W_{1_{x}} \\
W_{1_{y}} \\
Z_{1_{x}} \\
Z_{1_{y}}
\end{array}\right]=\left[\begin{array}{c}
E \\
L \\
M \\
N
\end{array}\right]
$$

## Example: Problem: 5-11 p. 255

Design a linkage to carry the bady in the figure below through the three positions Pl, P2 and P3 at the angles shown in the figure. Use analytical synthesis and design it for the fixed pivats shown.


## Example Solution - Step I

Determine the angle changes between precision points from the body angles given.

$$
\begin{array}{ll}
\alpha_{2}:=\theta_{P 2}-\theta_{P 1} & \alpha_{2}=-62.500 \mathrm{deg} \\
\alpha_{3}:=\theta_{P 3}-\theta_{P 1} & \alpha_{3}=-99.800 \mathrm{deg}
\end{array}
$$



## Example Solution - Step 2

determine the magnitudes of $\mathbf{R}_{1}, \mathbf{R}_{2}$, and $\mathbf{R}_{3}$ and their $x$ and $y$ components.

$$
\begin{array}{ll}
R_{l x}:=-O_{2 x} & R_{l x}=2.164 \\
R_{2 x}:=R_{l x}+P_{2 l x} & R_{2 x}=0.928 \\
R_{2 y}:=R_{l y}+P_{2 l y} & R_{2 y}=3.398 \\
R_{3 x}:=R_{l x}+P_{3 l x} & R_{3 x}=-0.336 \\
R_{3 y}:=R_{l y}+P_{3 l y} & R_{3 y}=4.191 \\
R_{1}:=\sqrt{R_{l x}^{2}+R_{l y}^{2}} & R_{1}=2.504 \\
R_{2}:=\sqrt{{R_{2 x}}^{2}+R_{2 y}^{2}} & R_{2}=3.522 \\
R_{3}:=\sqrt{R_{3 x}^{2}+R_{3 y}^{2}} & R_{3}=4.204
\end{array}
$$

$$
R_{I y}:=-O_{2 y}
$$

$$
R_{I y}=1.260
$$



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## Example Solution - Step 3

determine the angles that $\mathbf{R}_{1}, \mathbf{R}_{2}$, and $\mathbf{R}_{3}$ make with the $x$ axis.
$\zeta_{1}:=\operatorname{atan} 2\left(R_{l x}, R_{l y}\right)$
$\zeta_{1}=30.210 \mathrm{deg}$
$\zeta_{2}:=\operatorname{atan} 2\left(R_{2 x}, R_{2 y}\right)$
$\zeta_{2}=74.725 \mathrm{deg}$
$\zeta_{3}:=\operatorname{atan} 2\left(R_{3 x}, R_{3 y}\right)$
$\zeta_{3}=94.584 \mathrm{deg}$


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## Example Solution - Step 4a

## Solve for $\beta_{2}$ and $\beta_{3}$

$$
\begin{array}{ll}
C_{I}:=R_{3} \cdot \cos \left(\alpha_{2}+\zeta_{3}\right)-R_{2} \cdot \cos \left(\alpha_{3}+\zeta_{2}\right) & C_{1}=0.372 \\
C_{2}:=R_{3} \cdot \sin \left(\alpha_{2}+\zeta_{3}\right)-R_{2} \cdot \sin \left(\alpha_{3}+\zeta_{2}\right) & C_{2}=3.726 \\
C_{3}:=R_{1} \cdot \cos \left(\alpha_{3}+\zeta_{1}\right)-R_{3} \cdot \cos \left(\zeta_{3}\right) & C_{3}=1.209 \\
C_{4}:=-R_{I} \cdot \sin \left(\alpha_{3}+\zeta_{1}\right)+R_{3} \cdot \sin \left(\zeta_{3}\right) & C_{4}=6.538 \\
C_{5}:=R_{1} \cdot \cos \left(\alpha_{2}+\zeta_{1}\right)-R_{2} \cdot \cos \left(\zeta_{2}\right) & C_{5}=1.189 \\
C_{6}:=-R_{I} \cdot \sin \left(\alpha_{2}+\zeta_{1}\right)+R_{2} \cdot \sin \left(\zeta_{2}\right) & C_{6}=4.736
\end{array}
$$



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## Example Solution - Step 4b

## Solve for $\beta_{2}$ and $\beta_{3}$

| $A_{1}:=-C_{3}{ }^{2}-C_{4}{ }^{2}$ | $A_{1}=-44.206$ |
| :--- | :--- |
| $A_{2}:=C_{3} \cdot C_{6}-C_{4} \cdot C_{5}$ | $A_{2}=-2.046$ |
| $A_{3}:=-C_{4} \cdot C_{6}-C_{3} \cdot C_{5}$ | $A_{3}=-32.399$ |
| $A_{4}:=C_{2} \cdot C_{3}+C_{7} \cdot C_{4}$ | $A_{4}=6.937$ |
| $A_{5}:=C_{4} C_{5}-C_{3} \cdot C_{6}$ | $A_{5}=2.046$ |
| $A_{6}:=C_{7} C_{3}-C_{2} \cdot C_{4}$ | $A_{6}=-23.911$ |
| $K_{1}:=A_{2} \cdot A_{4}+A_{3} \cdot A_{6}$ | $K_{1}=760.497$ |
| $K_{2}:=A_{3} \cdot A_{4}+A_{5} \cdot A_{6}$ | $K_{2}=-273.669$ |
| $K_{3}:=\frac{A_{1}{ }^{2}-A_{2}{ }^{2}-A_{3}{ }^{2}-A_{4}{ }^{2}-A_{6}{ }^{2}}{2}$ | $K_{3}=140.232$ |



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## Example Solution - Step 4г

## Solve for $\beta_{2}$ and $\beta_{3}$

$$
\begin{aligned}
& \beta_{31}:=2 \cdot \operatorname{atan}\left(\frac{K_{2}+\sqrt{K_{1}^{2}+K_{2}^{2}-K_{3}^{2}}}{K_{l}+K_{3}}\right) \\
& \beta_{32}=2 \cdot \operatorname{atan}\left(\frac{K_{2}-\sqrt{K_{1}^{2}+K_{2}^{2}-K_{3}^{2}}}{K_{l}+K_{3}}\right)
\end{aligned}
$$

$$
\beta_{31}=60.217 \mathrm{deg}
$$

The second value is the same as $\alpha_{3}$, so use the first value

$$
\begin{aligned}
& \beta_{21}:=\operatorname{acos}\left(\frac{A_{5} \cdot \sin \left(\beta_{3}\right)+A_{3} \cdot \cos \left(\beta_{3}\right)+A_{6}}{A_{1}}\right) \\
& \beta_{22}:=\operatorname{asin}\left(\frac{A_{3} \cdot \sin \left(\beta_{3}\right)+A_{2} \cdot \cos \left(\beta_{3}\right)+A_{4}}{A_{1}}\right)
\end{aligned}
$$

$$
\beta_{21}=30.143 \mathrm{deg}
$$

$$
\beta_{22}=30.143 \mathrm{deg}
$$

Since both values are the same,
$\beta_{2}:=\beta_{21}$

## Example Solution - Step 5

Repeat steps 2,3, and 4 for the right-hand dyad to find $\gamma_{1}$ and $\gamma_{2}$.
$R_{1 x}:=-O_{4 x}$

$$
R_{I x}=-2.190
$$

$R_{l y}:=-O_{4 y} \quad R_{l y}=1.260$
$R_{2 x}:=R_{I x}+P_{2 I x}$
$R_{2 x}=-3.426$
$R_{2 y}:=R_{l y}+P_{2 l y}$
$R_{2 y}=3.398$
$R_{3 x}:=R_{I x}+P_{31 x}$
$R_{3 x}=-4.690$
$R_{3 y}:=R_{l y}+P_{3 l y}$
$R_{3 y}=4.191$
$R_{l}:=\sqrt{{R_{l x}}^{2}+R_{l y}{ }^{2}}$
$R_{1}=2.527$
$R_{2}:=\sqrt{R_{2 x}{ }^{2}+R_{2 y}{ }^{2}}$
$R_{2}=4.825$
$R_{3}:=\sqrt{R_{3 x}{ }^{2}+R_{3 y}{ }^{2}}$
$R_{3}=6.290$

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## Example Solution - Step B

determine the angles that $\mathbf{R}_{1}, \mathbf{R}_{2}$, and $\mathbf{R}_{3}$ make with the $x$ axis.

$$
\begin{aligned}
& \zeta_{1}:=\operatorname{atan} 2\left(R_{l x}, R_{l y}\right) \\
& \zeta_{2}:=\operatorname{atan} 2\left(R_{2 x}, R_{2 y}\right) \\
& \zeta_{3}:=\operatorname{atan} 2\left(R_{3 x}, R_{3 y}\right) \\
& \zeta_{1}=150.086 \mathrm{deg} \\
& \zeta_{2}=135.235 \mathrm{deg} \\
& \zeta_{3}=138.216 \mathrm{deg}
\end{aligned}
$$



## Example Solution - Step 7a

Solve for $\gamma_{2}$ and $\gamma_{3}$

$$
\begin{array}{ll}
C_{1}:=R_{3} \cdot \cos \left(\alpha_{2}+\zeta_{3}\right)-R_{2} \cdot \cos \left(\alpha_{3}+\zeta_{2}\right) & C_{1}=-2.380 \\
C_{2}:=R_{3} \cdot \sin \left(\alpha_{2}+\zeta_{3}\right)-R_{2} \cdot \sin \left(\alpha_{3}+\zeta_{2}\right) & C_{2}=3.298 \\
C_{3}:=R_{1} \cdot \cos \left(\alpha_{3}+\zeta_{1}\right)-R_{3} \cdot \cos \left(\zeta_{3}\right) & C_{3}=6.304 \\
C_{4}:=-R_{1} \cdot \sin \left(\alpha_{3}+\zeta_{1}\right)+R_{3} \cdot \sin \left(\zeta_{3}\right) & C_{4}=2.247 \\
C_{5}:=R_{1} \cdot \cos \left(\alpha_{2}+\zeta_{1}\right)-R_{2} \cdot \cos \left(\zeta_{2}\right) & C_{5}=3.532 \\
C_{6}:=-R_{1} \cdot \sin \left(\alpha_{2}+\zeta_{1}\right)+R_{2} \cdot \sin \left(\zeta_{2}\right) & C_{6}=0.874
\end{array}
$$

## Example Solution - Step 7b

$$
\begin{array}{ll}
A_{1}:=-C_{3}{ }^{2}-C_{4}{ }^{2} & A_{1}=-44.796 \\
A_{2}:=C_{3} C_{6}-C_{4} \cdot C_{5} & A_{2}=-2.431 \\
A_{3}:=-C_{4} \cdot C_{6}-C_{3} \cdot C_{5} & A_{3}=-24.233 \\
A_{4}:=C_{2} C_{3}+C_{7} \cdot C_{4} & A_{4}=15.441 \\
A_{5}:=C_{4} C_{5}-C_{3} \cdot C_{6} & A_{5}=2.431 \\
A_{6}:=C_{T} C_{3}-C_{2} \cdot C_{4} & A_{6}=-22.414 \\
K_{1}:=A_{2} A_{4}+A_{3} \cdot A_{6} & K_{1}=505.612 \\
K_{2}:=A_{3} A_{4}+A_{5} A_{6} & K_{2}=-428.679 \\
K_{3}:=\frac{A_{1}^{2}-A_{2}^{2}-A_{3}^{2}-A_{4}{ }^{2}-A_{6}{ }^{2}}{2} & K_{3}=336.363
\end{array}
$$

## Example Solution - Step 7c

$$
\begin{aligned}
& \gamma_{31}:=2 \cdot \operatorname{atan}\left(\frac{K_{2}+\sqrt{K_{I}^{2}+K_{2}^{2}-K_{3}^{2}}}{K_{I}+K_{3}}\right) \\
& \gamma_{32}:=2 \cdot \operatorname{atan}\left(\frac{K_{2}-\sqrt{K_{I}^{2}+K_{2}^{2}-K_{3}^{2}}}{K_{I}+K_{3}}\right)
\end{aligned}
$$

$\gamma_{31}=19.215 \mathrm{deg}$
$\gamma_{32}=-99.800 \mathrm{deg}$

The second value is the same as $\alpha_{3}$, so use the first value

$$
\begin{aligned}
& \gamma_{21}:=\operatorname{acos}\left(\frac{A_{5} \cdot \sin \left(\gamma_{3}\right)+A_{3} \cos \left(\gamma_{3}\right)+A_{6}}{A_{1}}\right) \\
& \gamma_{22}:=\operatorname{asin}\left(\frac{A_{3} \cdot \sin \left(\gamma_{3}\right)+A_{2} \cdot \cos \left(\gamma_{3}\right)+A_{4}}{A_{1}}\right)
\end{aligned}
$$

$$
\gamma_{21}=6.628 \mathrm{deg}
$$

$$
\gamma_{22}=-6.628 \mathrm{deg}
$$

Since $\gamma_{2}$ is not in the first quadrant,

$$
\gamma_{2}:=\gamma_{22}
$$

## Example Solution - Step 8

Solve for the linkage vectors as described on slide ill.
Start by finding the magnitudes of vectors $\mathrm{P}_{21}$ and $\mathrm{P}_{31}$ and its angles:

$$
\begin{array}{ll}
p_{21}:=\sqrt{P_{2 I x}^{2}+P_{2 l y}^{2}} & p_{21}=2.470 \\
\delta_{2}:=\operatorname{atan} 2\left(P_{2 I x}, P_{2 l y}\right) & \delta_{2}=120.033 \mathrm{deg} \\
p_{31}:=\sqrt{P_{3 I x}^{2}+P_{3 l y}^{2}} & p_{31}=3.852 \\
\delta_{3}:=\operatorname{atan} 2\left(P_{3 l x}, P_{3 l y}\right) & \delta_{3}=130.463 \mathrm{deg}
\end{array}
$$

## Example Solution - Step I

## Evaluate terms in the WZ coefficient matrix

$$
\begin{array}{lll}
A:=\cos \left(\beta_{2}\right)-1 & B:=\sin \left(\beta_{2}\right) & C:=\cos \left(\alpha_{2}\right)-1 \\
D:=\sin \left(\alpha_{2}\right) & E:=p_{2 I} \cdot \cos \left(\delta_{2}\right) & F:=\cos \left(\beta_{3}\right)-1 \\
G:=\sin \left(\beta_{3}\right) & H:=\cos \left(\alpha_{3}\right)-1 & N:=\sin \left(\alpha_{3}\right) \\
L:=p_{3 I} \cdot \cos \left(\delta_{3}\right) & M:=p_{2 r} \cdot \sin \left(\delta_{2}\right) & N:=p_{31} \cdot \sin \left(\delta_{3}\right) \\
A A:=\left(\begin{array}{cccc}
A & -B & C & -D \\
F & -G & H & -K \\
B & A & D & C \\
G & F & K & H
\end{array}\right) & C C:=\left(\begin{array}{c}
E \\
L \\
M \\
N
\end{array}\right) & \left(\begin{array}{c}
W l x \\
W l y \\
Z l x \\
Z l y
\end{array}\right):=A A^{-1} \cdot C C
\end{array}
$$

## Example Solution - Step 10

The components of the $W$ and $Z$ vectors are
$W 1 x=2.915$

$$
W l y=1.702
$$

$$
Z 1 x=-0.751
$$

$$
Z 1 y=-0.442
$$

And the length of link 2 is

$$
w:=\sqrt{W l x^{2}+W l y^{2}} \quad w=3.376
$$

## Example Solution - Step II

## Evaluate terms in the US coefficient matrix

$$
\begin{array}{lll}
A^{\prime}:=\cos \left(\gamma_{2}\right)-1 & B^{\prime}:=\sin \left(\gamma_{2}\right) & C:=\cos \left(\alpha_{2}\right)-1 \\
D:=\sin \left(\alpha_{2}\right) & E:=p_{2 I} \cdot \cos \left(\delta_{2}\right) & F^{\prime}:=\cos \left(\gamma_{3}\right)-1 \\
G^{\prime}:=\sin \left(\gamma_{3}\right) & H:=\cos \left(\alpha_{3}\right)-1 & K:=\sin \left(\alpha_{3}\right) \\
L:=p_{3 I} \cdot \cos \left(\delta_{3}\right) & M:=p_{2 I} \cdot \sin \left(\delta_{2}\right) & N:=p_{3 I} \cdot \sin \left(\delta_{3}\right) \\
A A:=\left(\begin{array}{cccc}
A^{\prime} & -B^{\prime} & C & -D \\
F^{\prime} & -G^{\prime} & H & -K \\
B^{\prime} & A^{\prime} & D & C \\
G^{\prime} & F^{\prime} & K & H
\end{array}\right) & C C:=\left(\begin{array}{c}
E \\
L \\
M \\
N
\end{array}\right)
\end{array}
$$

## Example Solution - Step 12

The components of the $ل$ and $S$ vectors are

Ulx $=-1.371 \quad$ Uly $=3.634 \quad$ Slx $=-0.819 \quad$ Sly $=-2.374$
And the length of link 4 is

$$
u:=\sqrt{U 1 x^{2}+U l y^{2}} \quad u=3.884
$$

## Example Solution - Step 13

Solving far links 3 and I

$$
\begin{array}{cl}
\qquad V l x:=Z l x-S l x & V l x=0.068 \\
V l y:=Z l y-S l y & V l y=1.932 \\
\text { The length of link } 3 \text { is: } \quad v:=\sqrt{V l x^{2}+V 1 y^{2}} & v=1.933
\end{array}
$$

$$
\begin{array}{ll}
G l x:=W l x+V l x-U l x & G l x=4.354 \\
G l y:=W l y+V l y-U l y & G l y=-4.441 \times 10^{-15}
\end{array}
$$

The length of link 1 is: $\quad g:=\sqrt{G l x^{2}+G l y^{2}} \quad g=4.354$

## Example Solution - Step 14

Check the location of the fixed pivat points with respect to the glabal frame using the calculated vectors WI, ZI, UI, and SI

$$
\begin{array}{ll}
O 2 x=-Z l x-\text { Wlx } & O 2 x=-2.164 \\
O 2 y=-Z l y-\text { Wly } & O 2 y=-1.260 \\
O 4 x=- \text { Slx } x-\text { Ulx } & O 4 x=2.190 \\
O 4 y=- \text { Sly } y-\text { Uly } & O 4 y=-1.260
\end{array}
$$

## Example Solution - Step 15

Determine the location of the coupler point with respect to point $A$ and line $A B$.

$$
\begin{array}{lll}
\text { Distance from } A \text { to } P & z:=\sqrt{Z l x^{2}+Z l y^{2}} & z=0.871 \quad r_{P}:=z \\
\text { Angle } B A P\left(\delta_{\mathrm{p}}\right) & s:=\sqrt{S 1 x^{2}+S l y^{2}} & s=2.511 \\
\psi:=\operatorname{atan} 2(S l x, S l y) & \psi=250.963 \mathrm{deg} \\
& \phi:=\operatorname{atan} 2(Z l x, Z l y) & \phi=210.445 \mathrm{deg} \\
\theta_{3}:=\operatorname{atan} 2(z \cdot \cos (\phi)-s \cdot \cos (\psi), z \cdot \sin (\phi)-s \cdot \sin (\psi)) \\
\theta_{3}=87.994 \operatorname{deg} & \\
\delta_{p}:=\phi-\theta_{3} & \delta_{p}=122.451 \mathrm{deg}
\end{array}
$$

## Example Solution - Summary

## DESIGN SUMMARY

| Link 1: | $g=4.354$ |
| :--- | :--- |
| Link 2: | $w=3.376$ |
| Link 3: | $v=1.933$ |
| Link 4: | $u=3.884$ |
| Coupler point: | $r_{P}=0.871 \quad \delta_{p}=122.451 \mathrm{deg}$ |

VERIFICATION: The calculated values of $g$ (length of the ground link) and of the coordinates of $O_{2}$ and $O_{4}$ give the same values as those on the problem statement, verifying that the calculated values for the other links and the coupler point are correct.

